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VELOCITY MEASUREMENT BY SCATTERING FROM INDEX OF REFRACTION FLUCTUATIONS INDUCED IN TURBULENT FLOWS

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Induced Phase Screen Scattering

What is it?

- Scatter light from from weak index of refraction fluctuations induced by turbulence.

Basic Assumptions and Requirements

- **Quasi-elastic interaction**
- **Weak interaction, i.e. $\langle (\Delta n)^2 \rangle \ll \langle n \rangle^2$**
- **The *probing scale* must be larger than the mean free path or the Debye length (plasma).**
- **Small scales are used to sample the dynamics of larger scales.**
- **The persistence time of the refractive index pattern must be longer than the residence time.**
- **The size of the measuring volume must be smaller than the scale to be measured.**

Scattering and detection:

Scale requirements $\Rightarrow$

forward scattering

far infrared light ($\lambda = 10 \mu\text{m}$)

Weak interaction $\Rightarrow$ infrared light (or shorter λ)

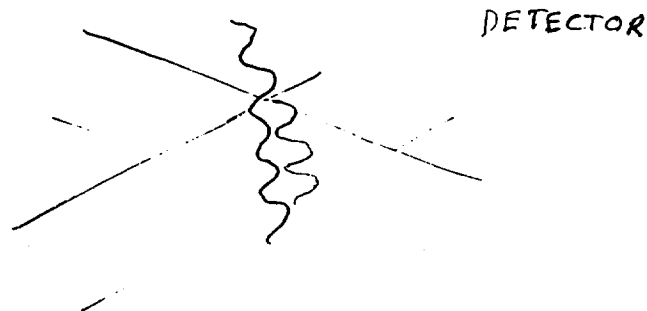
Coherent detection (phase fronts parallel over the detector area):

Reference beam detection because:

parametric amplification needed

simpler statistics

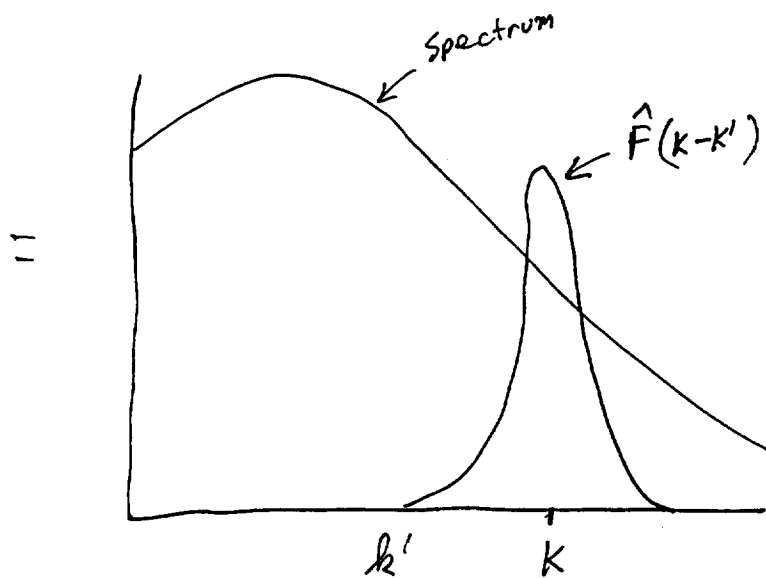
- . Scale selected in the usual way by heterodyne scattering angle and laser wavelength.



$$i(t) = \int e^{i\mathbf{k}\cdot\mathbf{r}} F(\mathbf{r}) S(\mathbf{r}, t) d\mathbf{r}$$

$$i(t) = \int \hat{F}(\mathbf{k} - \mathbf{k}') \hat{S}(\mathbf{k}') d\mathbf{k}'$$

$\hat{S}(\mathbf{k}')$ is the Fourier Transform of the spatial distribution of the scattering power.



Here, fluctuations are induced by turbulence itself - e.g. Noise is a manifestation of pressure fluctuations.

Temperature fluctuations can be induced by turbulence in a gas flow

Local electron number density can be induced by turbulence in a plasma.

Divide fluctuations into two types:

1) Propagating - Sound Waves

2) Non-propagating - Temperature Fluctuations

$$d\mathbf{n} = \beta_1 dT + \beta_2 dP$$

For a moving, compressible fluid

$$\rho \hat{C}_p \left(\frac{\partial (T - T_0)}{\partial t} + \mathbf{v} \cdot \nabla (T - T_0) \right) =$$

$$\alpha \rho \hat{C}_p \nabla^2 (T - T_0) - \left(\frac{\partial p}{\partial t} + \mathbf{v} \cdot \nabla p \right)$$

Take the spatial Fourier Transform

$$\frac{\partial \hat{\Theta}(\mathbf{k}, t + \tau)}{\partial \tau} - i \mathbf{k} \cdot \mathbf{v} \hat{\Theta}(\mathbf{k}, t + \tau) =$$

$$- k^2 \alpha \hat{\Theta}(\mathbf{k}, t + \tau) - \frac{p_0 \gamma \delta \omega}{2 \rho_0 \hat{C}_p} e^{-i \mathbf{k} \cdot (\mathbf{v} + \mathbf{v}_s)(t + \tau)}$$

The correlation function for the temperature fluctuations

$$C_{TT}(\mathbf{k}, \tau) \equiv \hat{\Theta}(\mathbf{k}, t) \hat{\Theta}(\mathbf{k}, t + \tau)$$

$$\frac{\partial C_{TT}(\mathbf{k}, \tau)}{\partial \tau} - i \mathbf{k} \cdot \mathbf{v} C_{TT}(\mathbf{k}, \tau) = -k^2 \alpha C_{TT}(\mathbf{k}, \tau)$$

$$C_{TT}(\mathbf{k}, \tau) = C_{TT}(\mathbf{k}, 0) \exp[i \mathbf{k} \cdot \mathbf{v} \tau] \exp[- k^2 \alpha \tau]$$

If we assume sound waves do not attenuate over scale of measurement,

$$C_{PP}(\tau) = \exp[i \mathbf{k} \cdot (\mathbf{v} \pm \mathbf{v}_s) \tau]$$

Overall

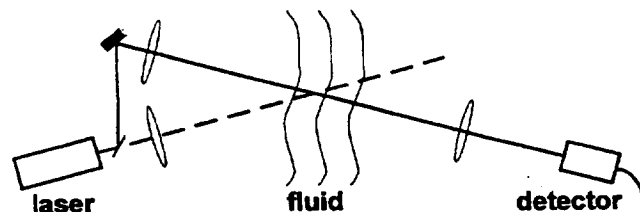
$$\hat{R}_{SS}(\mathbf{k}, \tau) = \varepsilon_1^2 \exp[- i \mathbf{k} \cdot \bar{\mathbf{v}} \tau] \exp[- k^2 \alpha \tau] + \varepsilon_2^2 \exp[- i \mathbf{k} \cdot (\bar{\mathbf{v}} \pm \mathbf{v}_s) \tau]$$

Note the thermal decay term.

For air, $\alpha \approx 0.1 \text{ cm}^2 \text{ sec}^{-1}$. If $k \approx 10^4 \text{ cm}^{-1}$, the decay time is ca. 0.1 microseconds!

Means that practical system will need small scattering angle.

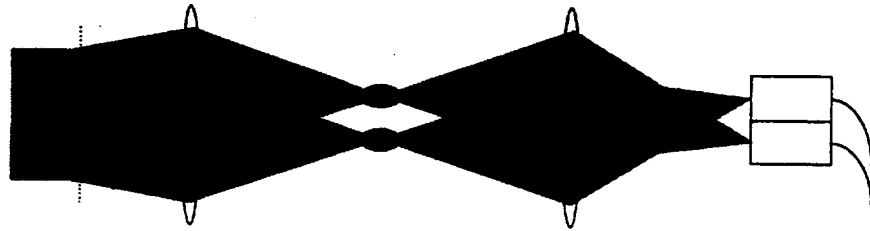
Doppler Velocimeter



The code of the system is a spatial wave packet.

The system has poor spatial resolution along the optical axis.

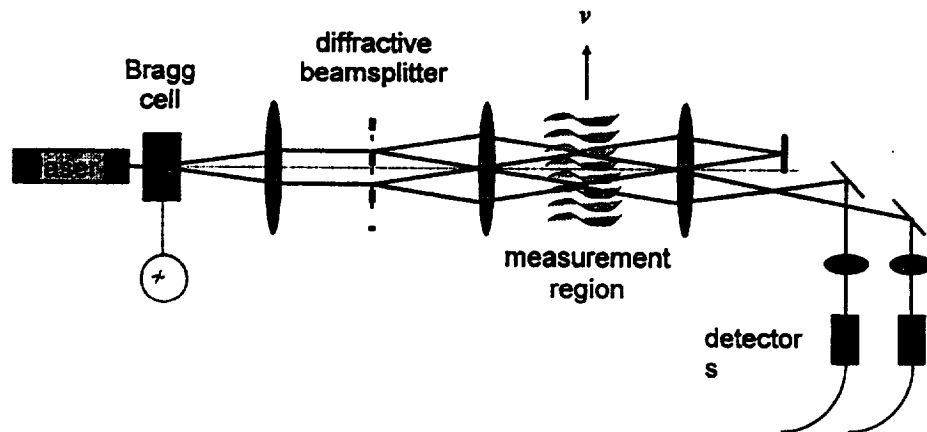
A time-of-flight configuration

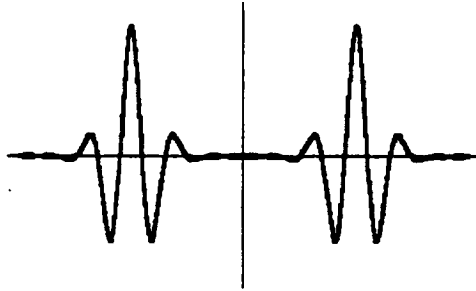


The code is given by two displaced peaks.

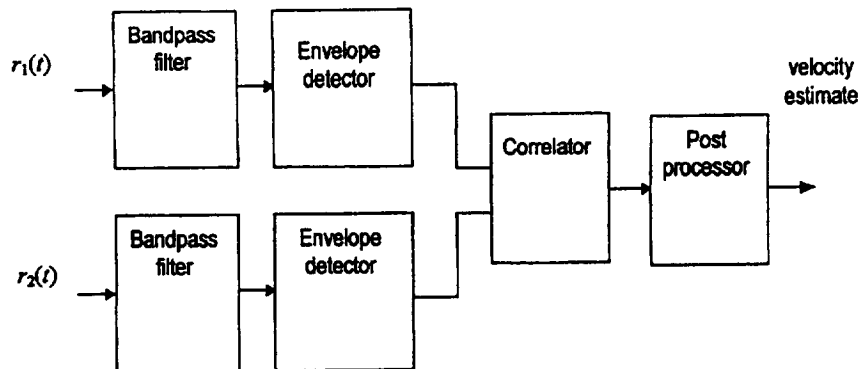
Has very good resolution along the optical axis - but
does not work in the present case!

The hybrid system





The intensity distribution (deviation from the mean) as seen by the detectors of a hybrid laser anemometer, which defines the *code* of the system.



Cross Correlation

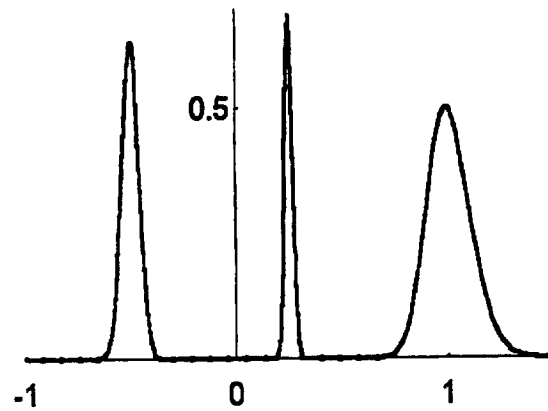
$$R_{12}(\tau) = \iint \hat{F}(k - k') \hat{F}(k - k'') e^{-i \mathbf{k}'' \cdot \mathbf{l}} \langle \hat{S}(k', t) \hat{S}(k'', t + \tau) \rangle dk' dk''$$

For turbulent flow

$$^{(2)}R_c(\tau) = \int_{\text{all } v} ^{(2)}R_{12}(\tau, v) dP(v)$$

Envelope detection is used, so

$$R(\tau) = R_{12}^2(0) + 2 R_{12}^2(\tau)$$



Correlation function assuming both propagating and nonpropagating fluctuations of the same initial power. The s.d. of the convection velocity is 0.1. The Mach # is 0.33.



Mach # of 4.

Conclusion + current state

- **Mean velocity + turbulence from peak + width of crosscorrelation if low turbulence intensity and well separated velocities**
- **Curve fitting is necessary in general**
- **Simplest if propagating fluctuations are negligible**
- **Optics of new system is operating and signals observed**